

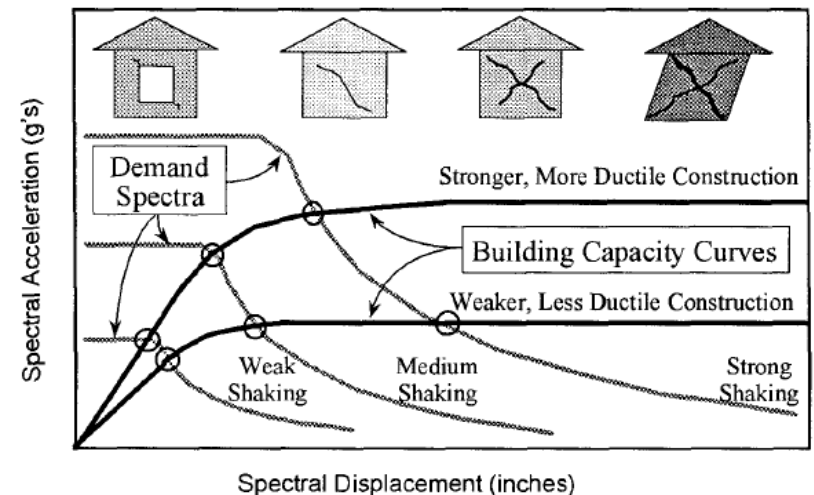
WHE-PAGER Project

Dr. Dina D' Ayala
Senior Lecturer



Seismic assessment of building stock and prediction of losses

- Input
 - Classification of buildings
 - Assignment of capacity curves
 - Definition of damage states
 - Definition of demand spectra
 - Evaluation of building response



- Output
 - Fragility curves
 - Damage scenarios



General Methodology

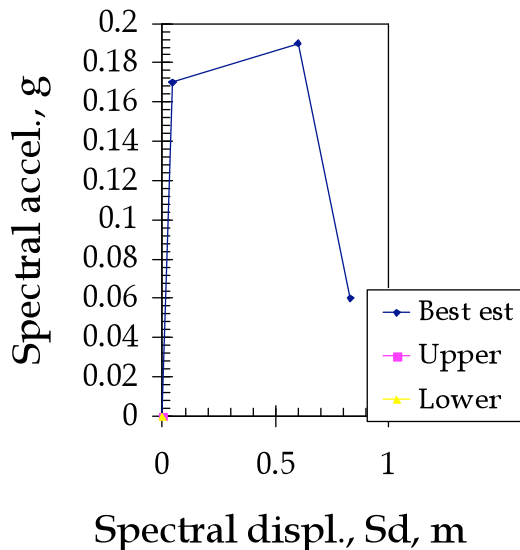
- Building classification by building typology
- If typologies are codified then capacity curves deduced from design standards
- Damage thresholds more difficult but theoretical correlation between damage and drift available for engineered structures
- Correlation of drift capacity and demand from displacement spectra possible
- Distribution of building stock from census by typology and use of lognormal distribution around mean average damage
- Possible calibration of fragility curves with direct damage observations and experimental work.

Request to the analytical



phase contributors

- Fill a spreadsheet providing a push over curve defining how far we are from the HAZUS approach



WHE-PAGER PHASE 2: DEVELOPMENT OF ANALYTICAL SEISMIC VULNERABILITY FUNCTIONS			
Author:	Hemant B. kaushik		
Date:	10-Jul-09		
Structure type (describe as broadly as possible):	Non-Ductile Reinforced Concrete Frame without Masonry Infill Walls		
Geographic or other limitations:	Northern India, Modern Building Construction		
	As per the prevalent method of design of such buildings in India, strength and stiffness of masonry infills is not considered (only) Add rows as desired		
Choice of pushover curve parameters			
Pushover X-axis:	Sd(m)	Parameter	Choose spectral displacement (Sd) or Roof displacement (Deltar). State units
Pushover Y-axis:	Sal(g)		Choose spectra acceleration (Sa), or base shear (V). State units.
Elastic damping ratio:	0.05		Small-amplitude damping ratio, fraction of critical
1st mode participation factor:	1.2		PF1R, generally 1.3 to 1.5, same as (effective height)/(total roof height)
Effective mass coefficient:	0.96		alpha1, generally 0.7 to 0.8
Building weight:	1640 kN	Weight of the W	State units
How were these values & pushover points derived?	Based on analytical simulations of an intermediate frame of a four storey building. Actual performance of real buildings may be different. Ref. Kaushik, H.B., Rai, D.C., and Jain, S.K. (2009). "Effectiveness of some strengthening options for masonry-infilled RC frame" Add rows as desired		
Pushover Curve for this structure type			
	See Figures 1-4 for sample pushover curves		
Pushover curve control point	X	Y	Damping
A	0	0	0.13
B	0.044	0.17	
C	0.6	0.19	
D	0.83	0.06	
E			
	Control point for plotting purposes		
	E.g., yield point?		
	E.g., ultimate point?		
	E.g., beginning of lower plateau?		
	Add rows as desired		
Optional: upper and lower-bound range of pushover curves for this structure type			
	Upper-bound pushover curve, e.g., 99 out of 100 buildings of this type would have pushover curve inside the area bounded between this curve and the Y-axis?		
Author's meaning of "upper bound":			
How were these values & pushover points derived?	Add rows as desired		
	See Figures 1-4 for sample pushover curves		
Optional upper-bound pushover curve			
Pushover curve control point	X	Y	Damping
A	0	0	
B			
C			
D			
E			
	Control point for plotting purposes		
	E.g., yield point?		
	E.g., ultimate point?		
	E.g., beginning of lower plateau?		
	Add rows as desired		
	Lower-bound pushover curve, e.g., 99 out of 100 buildings of this type would have pushover curve inside the area bounded between this curve and the X-axis?		
Author's meaning of "lower bound":			
How were these values & pushover points derived?	Add rows as desired		
	See Figures 1-4 for sample pushover curves		
Optional lower-bound pushover curve			
Pushover curve control point	X	Y	Damping
A	0	0	
B			
C			
D			
E			
	Control point for plotting purposes		
	E.g., yield point?		
	E.g., ultimate point?		
	E.g., beginning of lower plateau?		
	Add rows as desired		
Other requested parameters			
D14		median drift (in same units as pushover X-axis) associated with complete structural damage, i.e., drift with 50% chance that the structural com	
B14		logarithmic standard deviation of drift associated with complete structural damage. May need to be guessed	
Sdc		the median value of drift (in same units as pushover X-axis) associated with collapse. e.g., Sdc = (roof drift at collapse)/PF1R	
L15		indoor fatality rate given collapse. Many contributors may be unable to provide this value. Porter, Comartin, and Holmes will fill such gaps	
PC		mean fraction of building area collapsed, given complete structural damage. Again Porter, Comartin, and Holmes will fill gaps	
kshort		If HAZUS-style damping preferred, and author can judge, this is the degradation factor for short-duration (M <= 5.5) events	
kmed		If HAZUS-style damping preferred, and author can judge, this is the degradation factor for medium-duration (5.5 < M < 7.5) events	
klong		If HAZUS-style damping preferred, and author can judge, this is the degradation factor for long-duration (M >= 7.5) events	
Explain how these values were arrived at, providing citations if appropriate			
	Add rows as desired		



Analytical push-over curves for non-HAZUS structures types

- Identify experimental/analytical curves existing in literature
- Document type of test/analytical procedure, representativeness, etc.
- Use FaMIVE database to extract a number of region/structure specific curves
- Compare with curves in literature
- Produce fragility curves

PAGER Structure types considered

Sr. No.	PAGER-STR	Description of Structure
8	RS3	Local field stones with lime mortar.
9	RS4	Local field stones with cement mortar, vaulted brick roof and floors
10	DS2	Rectangular cut stone masonry block with lime mortar
11	DS4	Rectangular cut stone masonry block with reinforced concrete floors and roof
12	MS	Massive stone masonry in lime or cement mortar
14	UFB1	Unreinforced brick masonry in mud mortar without timber posts
15	UFB3	Unreinforced brick masonry in lime mortar
16	UFB5	Unreinforced fired brick masonry, cement mortar, but with reinforced concrete floor and roof slabs

Literature -Experimental



Earthquake Engineering
Research Institute

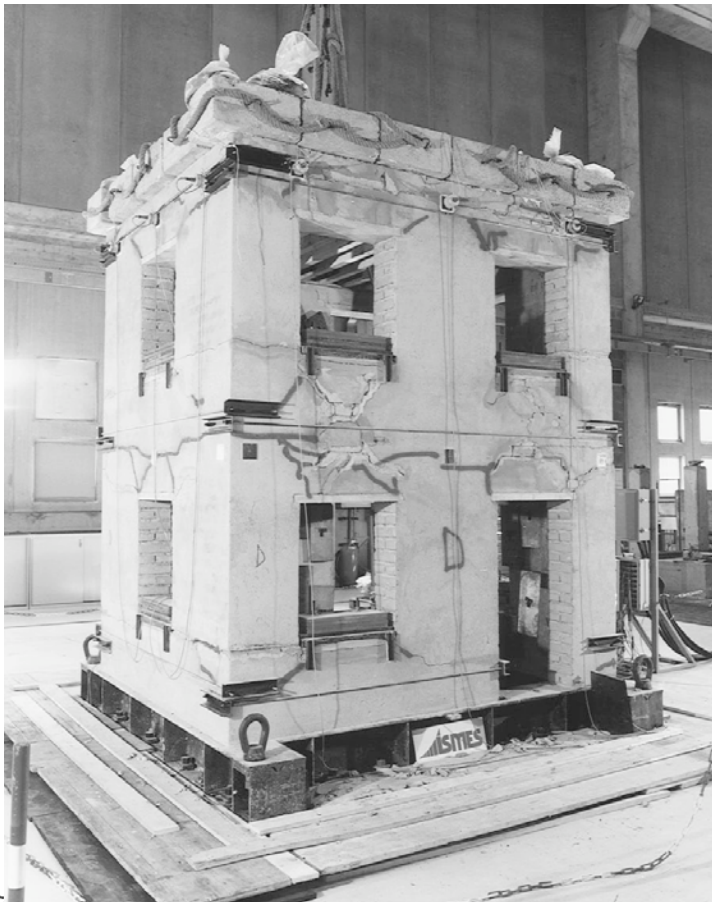
- [5] **Benedetti D., Carydis P., Pezzoli P., 1998**, ‘Shaking Table Tests on 24 Simple Masonry Buildings’ *Earthquake Engineering and Structural Dynamics*: Vol 27: 67-90
- [6] **Magenes G., Calvi G., 1997**, ‘In-Plane Seismic Response of Brick Masonry Walls’ *Earthquake Engineering and Structural Dynamics*: Vol 26: 1091-1112
- [7] **Tomazevic M.**, ‘Damage as a Measure for Earthquake-Resistant Design of Masonry Structures: Slovenian Experience’, *Can. J. Civ. Eng.* 34: 1403-1412, 2007
- [8] **Tomazevic M., Lutman M., Weiss M., Velechovsky T.**, ‘The Influence of Rigidity of Floors on the Seismic Resistance of Masonry Buildings: Shaking Table Tests of Stone Masonry Houses Summary Report’, *A Report to the Ministry of Science of Republic of Slovenia Institute for Testing and Research in Materials and Structures, Ljubljana, Slovenia, 1992*
- [10] **Paquette J., Bruneau M.**, ‘Pseudo Dynamic Testing of Unreinforced Masonry Building with Flexible Diaphragm’ *Journal of Structural Engineering*, ASCE, June 2003
- [11] **Yi T., Moon F., Leon R., Kahn L.**, ‘Lateral Load Tests on a Two Storey Unreinforced Masonry Building’ *Journal of Structural Engineering*: ASCE: May 2006
- [12] **Griffith M., Lam N., Wilson J., Doherty K.**, ‘Experimental Investigation of Unreinforced Brick Masonry Walls in Flexure’, *Journal of Structural Engineering*, ASCE, March 2004: 423-432
- [13] **Doherty K., Griffith M., Lam N., Wilson J.**, ‘Displacement-Based Seismic Analysis for Out-of-Plane Bending of Unreinforced Masonry Walls’, *Earthquake Engineering and Structural Dynamics*: 2002: 31: 833-850
- [14] **Degée H., Denoël V., Candeias P., Campos Costa A., Coelho E.**, ‘Experimental Investigation on the Seismic Behaviour of North European Masonry Houses’, *Sismica 2007- 7º Congresso de Sismologia Engenharia Sismica*



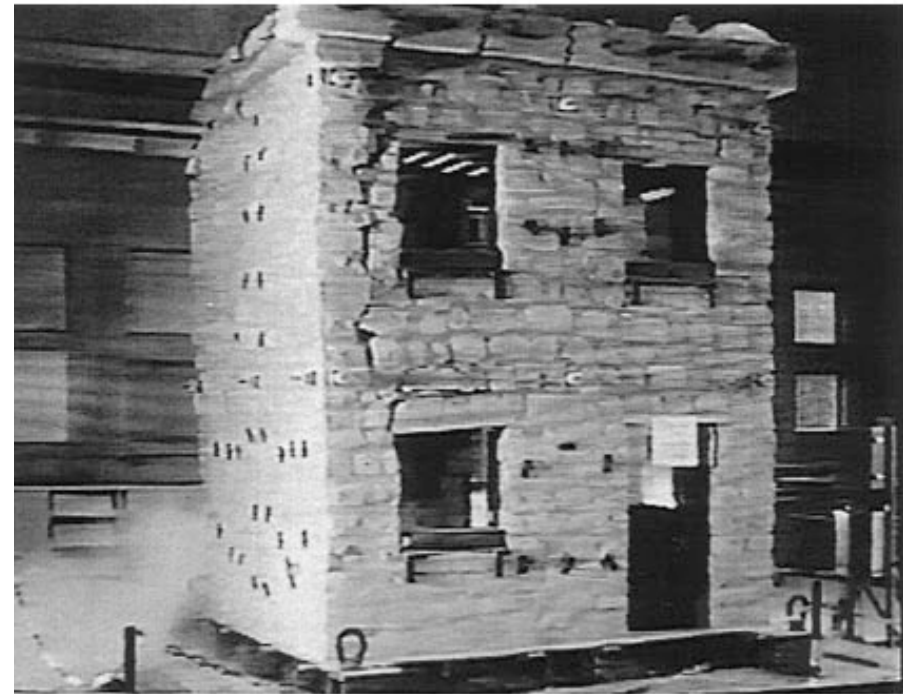
Department of Architecture and Civil Engineering
University of Bath

Benedetti et al. 1998

Brick masonry UFB3

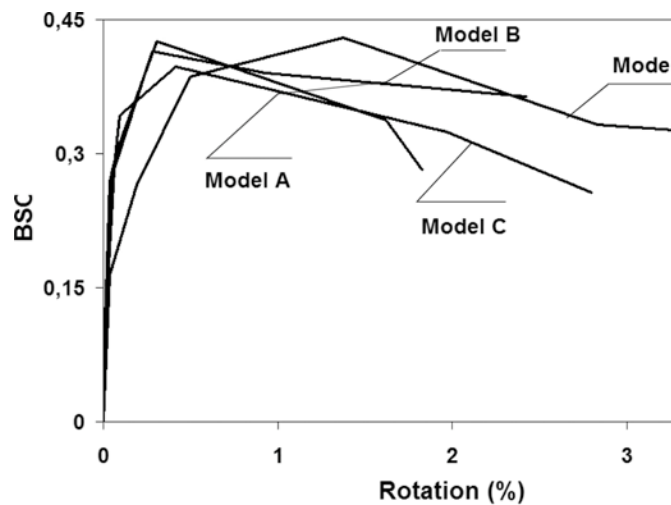


Rubble masonry DS2

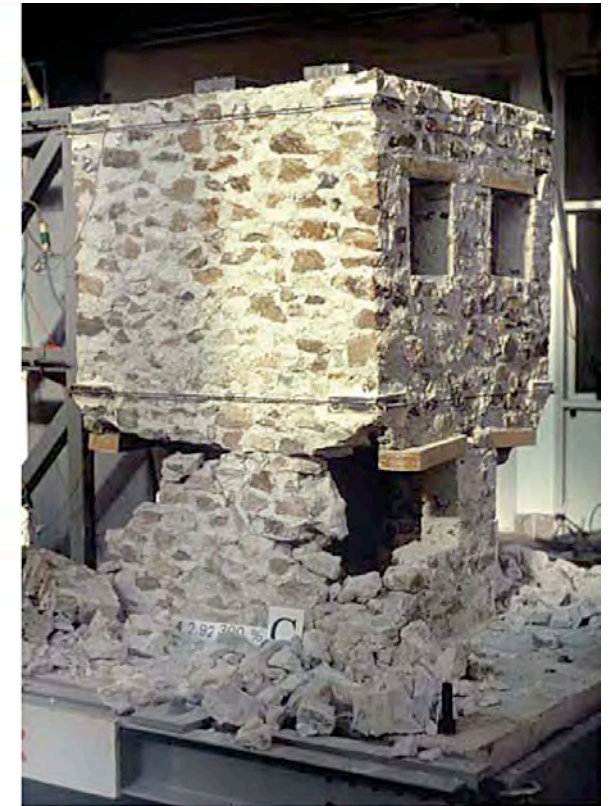


Tomazevic & Lutman 2004

Rubble stone
RS4



Model A: without wall ties

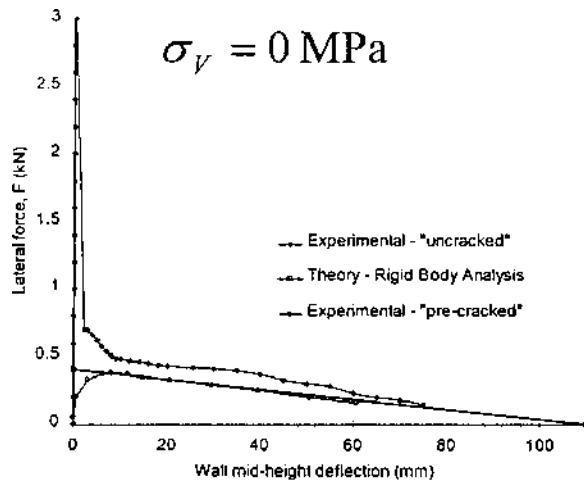


Model C: with wall ties

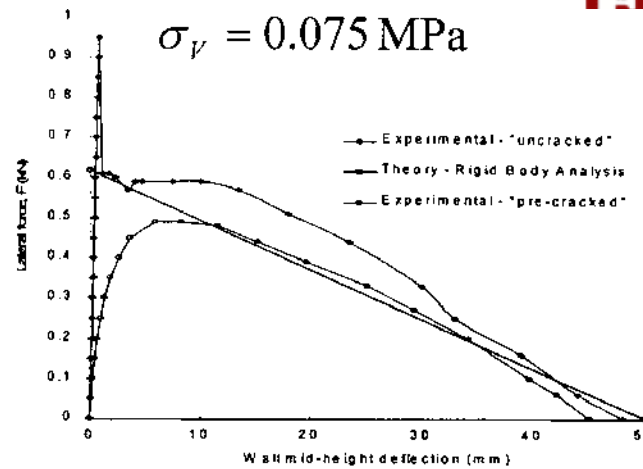
Literature Analytical

- [15] **D'Ayala D., 2005**, 'Force and Displacement Based Vulnerability Assessment for Traditional Buildings', *Bulletin of Earthquake Engineering*: 2005:3:235-265
- [16] **Cattari S., Lagomarsino S., 2006**, 'Non-Linear Analysis of Mixed Masonry and Reinforced Concrete Buildings', *First European Conference on Earthquake Engineering and Seismology, Geneva, Switzerland, 3-8th September 2006*: Paper no. 927
- [17] **Penelis G.**, 'An Efficient Approach for Pushover Analysis of Unreinforced Masonry (URM) Structures', *Journal of Earthquake Engineering*: Vol 10: No.3: 2006: 359-379
- [18] **Penelis G., Kappos A., Stylianidis K., 2003**, 'Assessment of the seismic vulnerability of unreinforced masonry buildings', *Structural Studies, Repairs and Maintenance of Heritage Architecture VIII*: 575-584
- [19] **Salonikios T., Karakostas C., Lekidis V., Anthoine A.**, 'Comparative Inelastic Pushover Analysis of Masonry Frames', *Engineering Structures* 25: 2003: 1515-1523
- [20] **Kappos A., Panagopoulos G., Panagiotopoulos C., Penelis G.**, 'A Hybrid Method Method for the Vulnerability Assessment of RC and URM Buildings', *Bull Earthquake Eng*: (2006): 4: 391-413
- [21] **Barbat A.**, 'Performance of Buildings Under Earthquakes in Barcelona, Spain', *Computer-Aided Civil and Infrastructure Engineering*: 21: (2006): 573-593

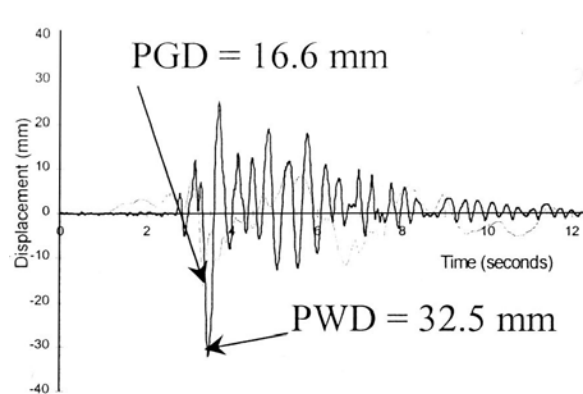
Griffith et al. (2004)



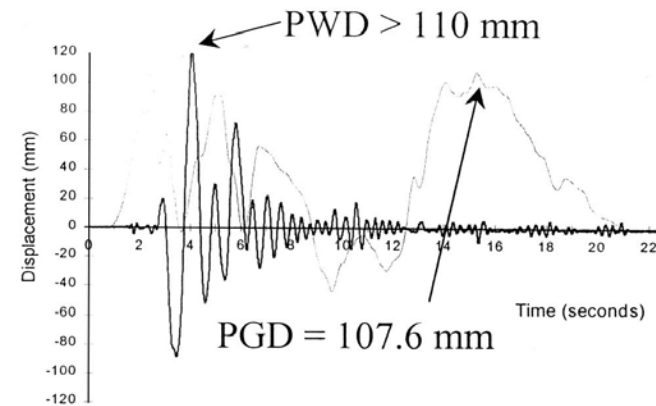
(a) 110 mm thick wall



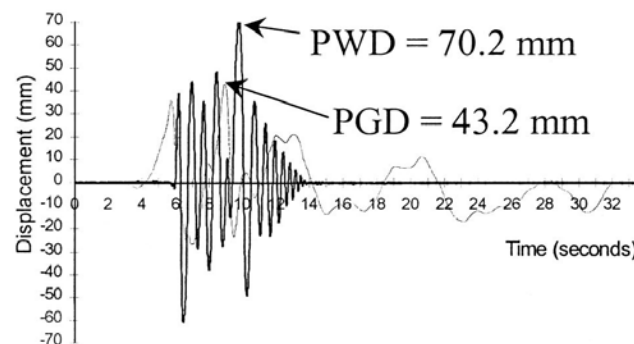
(b) 50 mm thick wall



(a) 4 x Nahini



(b) 0.66 x El Centro



(c) 0.8 x Pacoima Dam



Regions

- Italy



Turkey



- Iraq

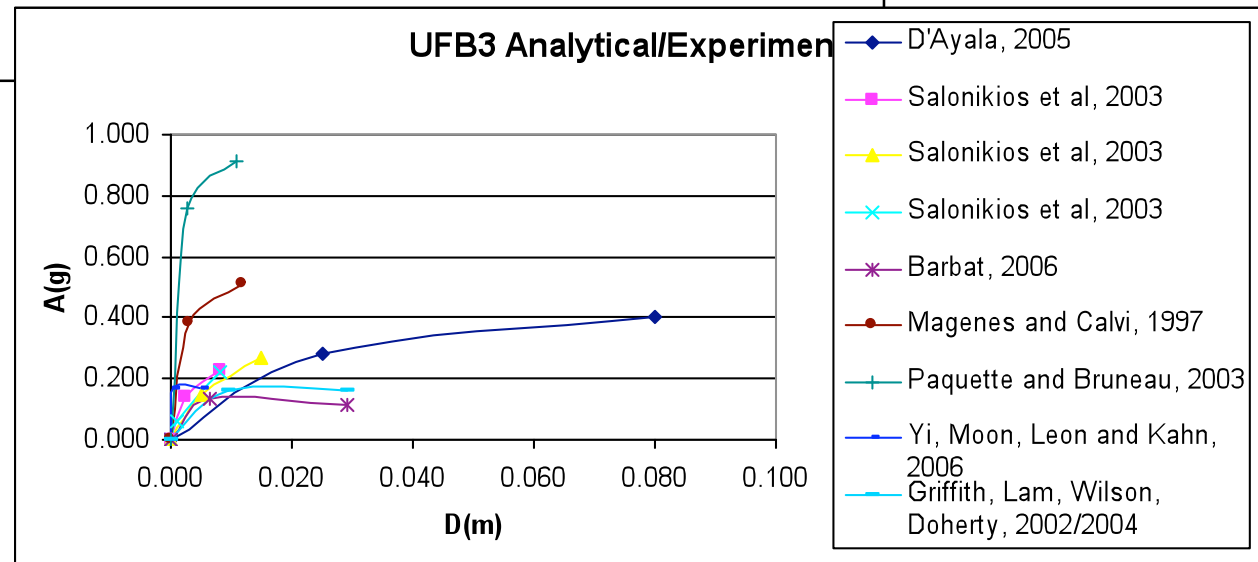
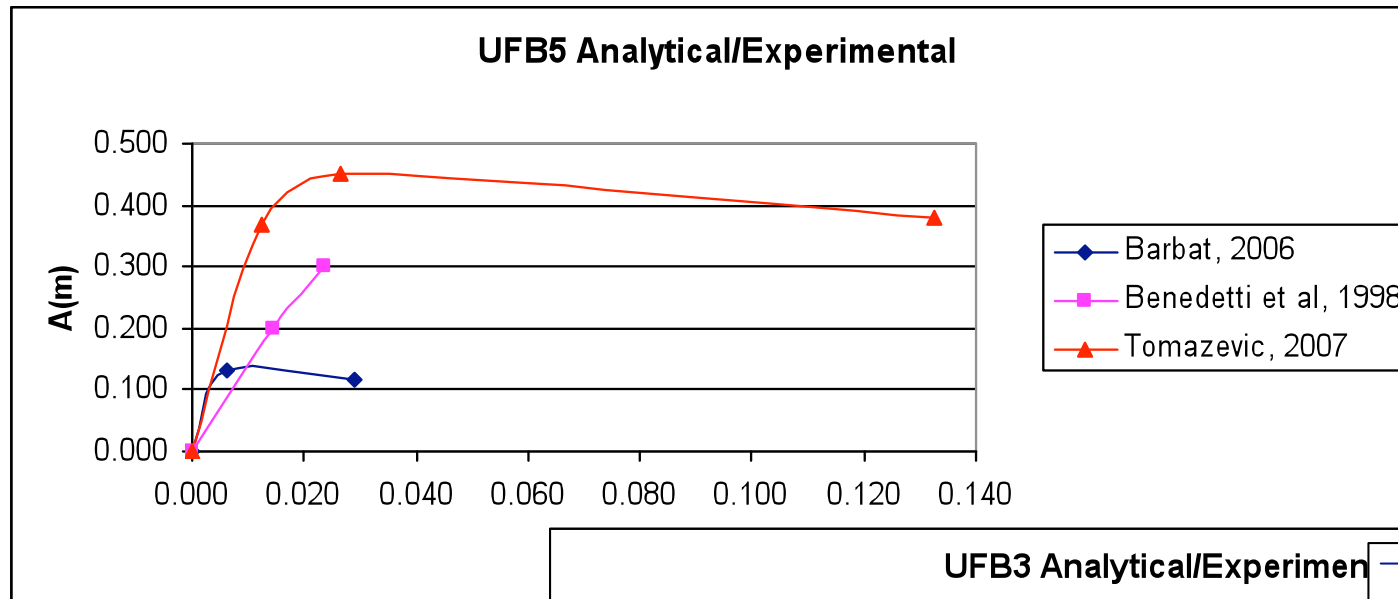


Nepal





Literature Push-over Curves



Mechanisms of collapse

- Friction, identification of cracks by sliding or overturning
- Connections with other structural elements

A	B1	B2	C	D	E	F
VERTICAL OVERTURNING	OVERTURNING WITH 1 SIDE WING	OVERTURNING WITH 2 SIDE WINGS	CORNER FAILURE	PARTIAL OVERTURNING	VERTICAL STRIP OVERTURNING	VERTICAL ARCH
				ASSOCIATED FAILURES		
G	H	I	H2			M
HORIZONTAL ARCH	IN PLANE FAILURE	VERTICAL ADDITION	IN PLANE PIER FAILURE	ROOF/FLOORS COLLAPSE	MASONRY FAILURE	SOFT STOREY

Displacement based assessment

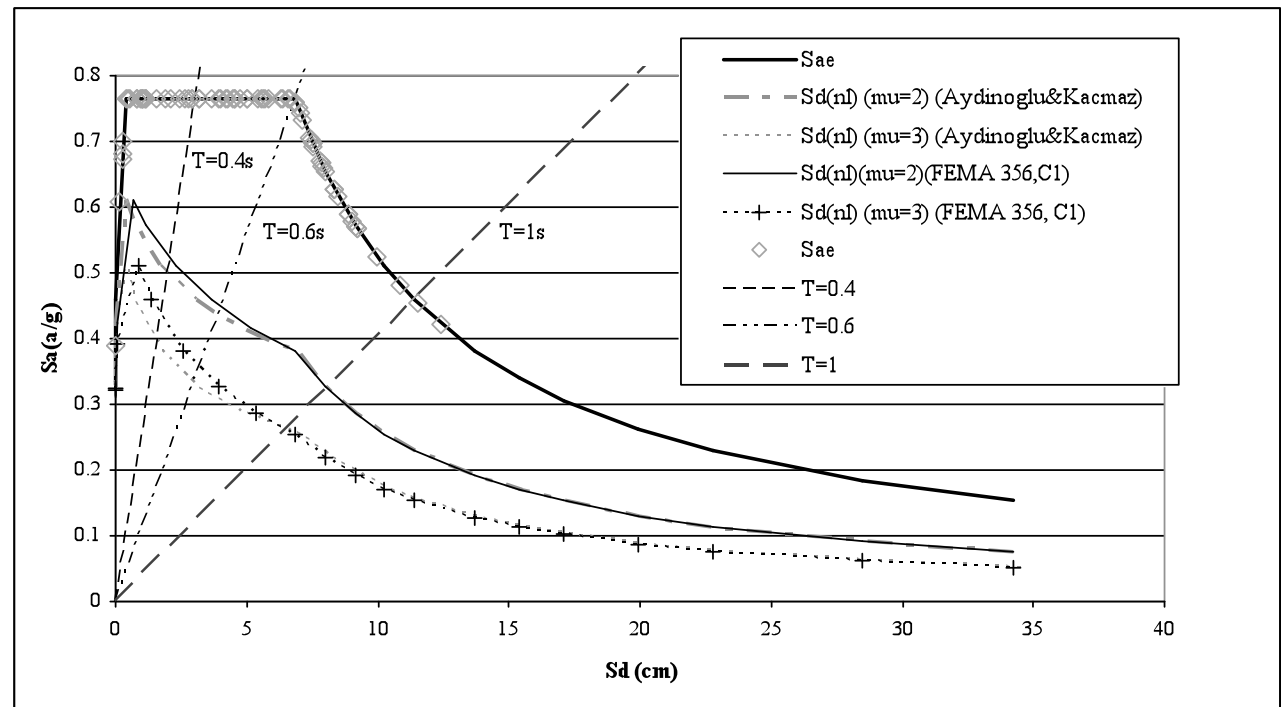


- Choice of appropriate non linear spectrum:
 - Deterministic event \Rightarrow site specific PGA
 - Ductility \Rightarrow Strength reduction factor
 - Displacement reduction factors:

$$R = \begin{cases} c_1(\mu - 1)\frac{T}{T_g} + 1 & \frac{T}{T_g} \leq 1 \\ c_1(\mu - 1) + 1 & \frac{T}{T_g} > 1 \end{cases}$$

$$S_{dar} = \begin{cases} [1 + (R - 1)T_g / T] R & T < T_g \\ 1 & T > T_g \end{cases}$$

$$S_{dar} = 1 + \frac{(R_y - 1)^2}{300} + \frac{1}{10T^2} e^{-20\frac{\sqrt{T}}{R_y}}$$



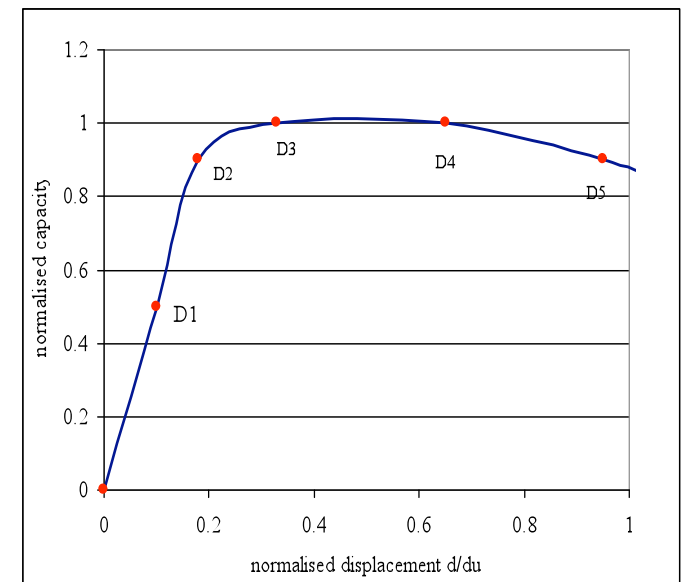
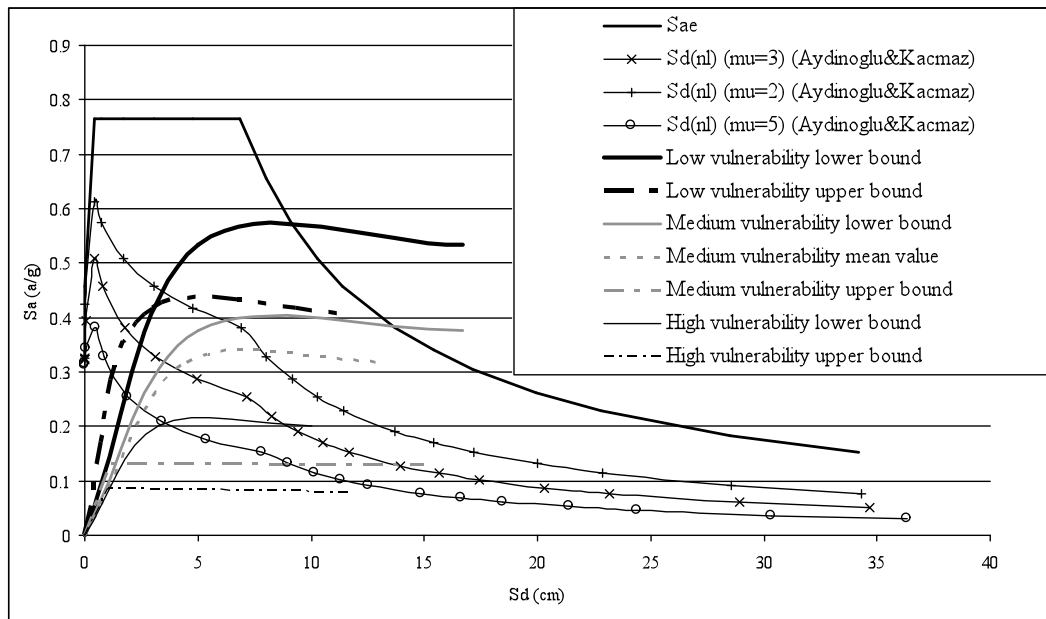
Capacity curves for vulnerability classes

- Define peak strength as collapse load factor
- Define natural period as ratio of effective stiffness and mass
- Define elastic limit displacement as
- Define Δ_u as loss of equilibrium for given mechanism
- Typical ductility range $3 < \mu < 10$

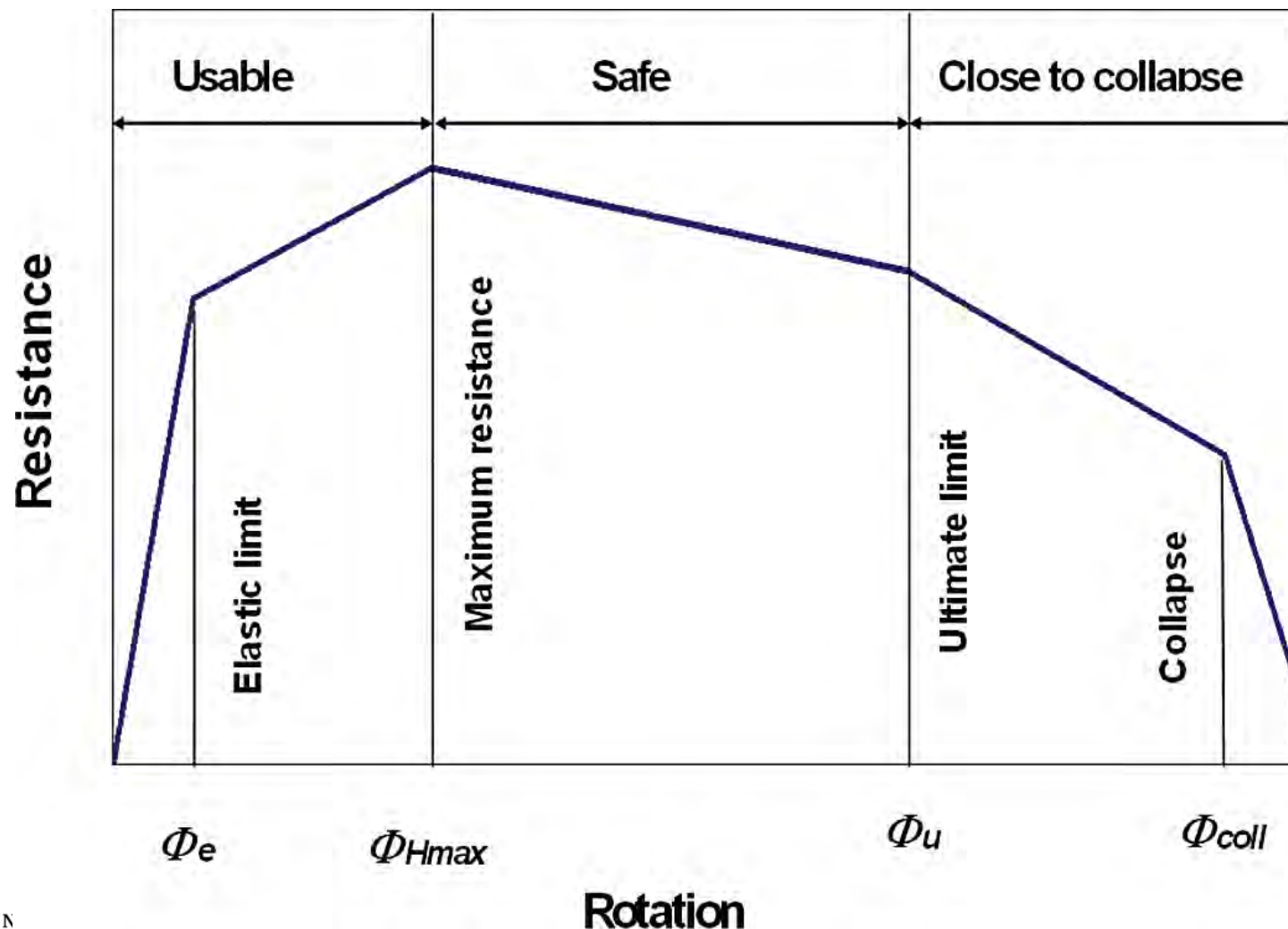
$$a_y = \lambda$$

$$T = \sqrt{\frac{m_{eff}}{K_{eff}}}$$

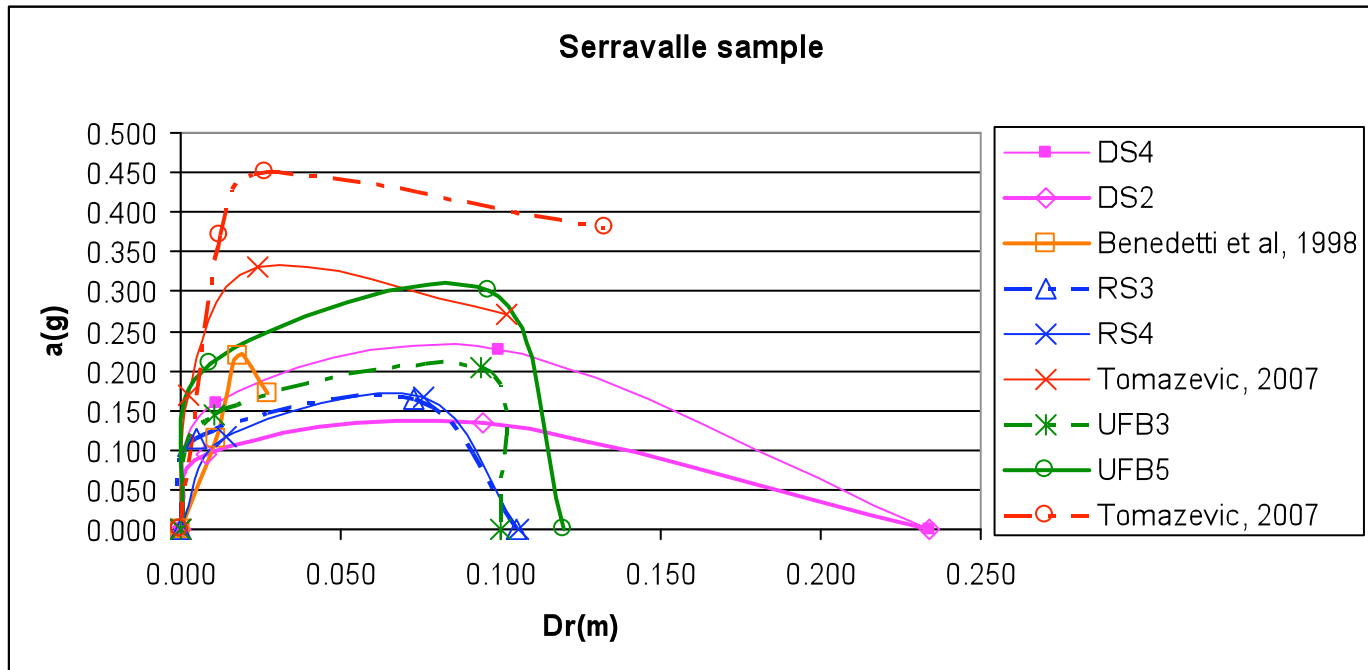
$$\Delta_y = \frac{a_y}{4\pi^2} T^2$$



Tomazevic & Lutman 2004

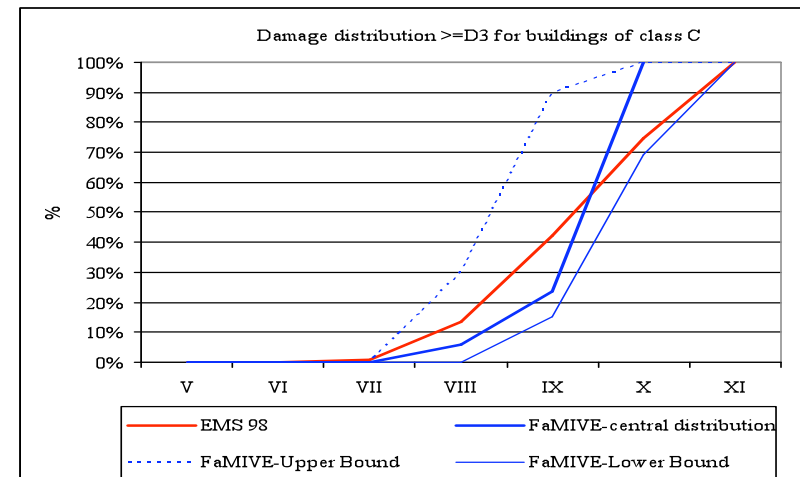
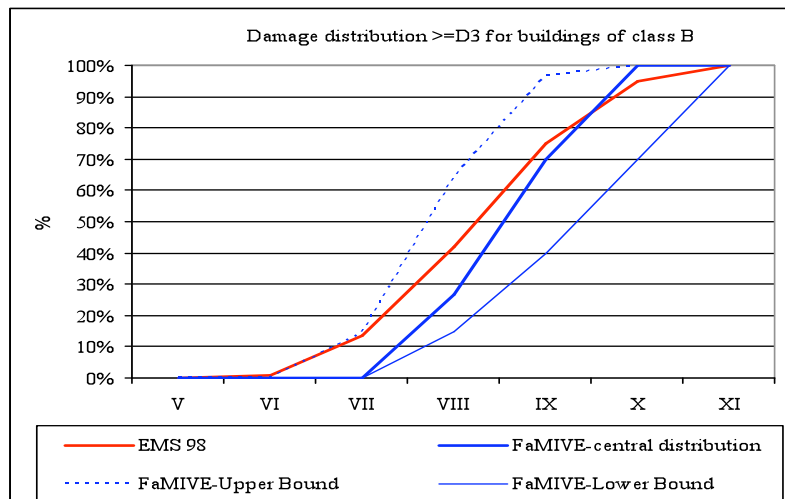
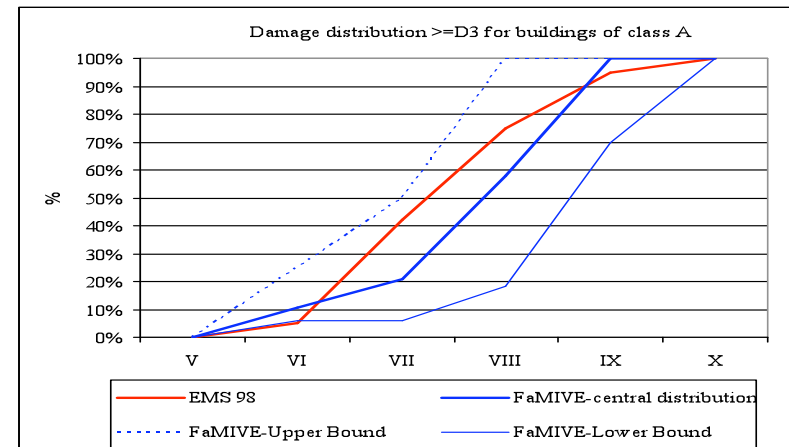


Italy, Serravalle

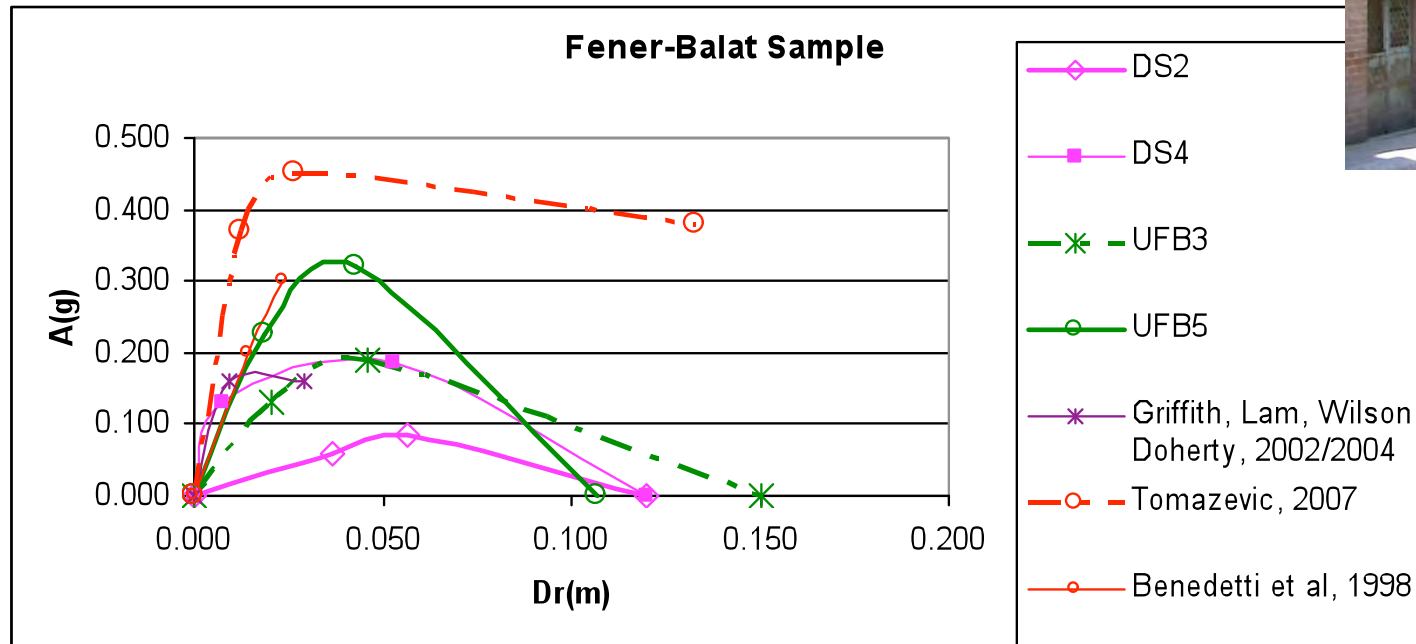


Serravalle, Italy, Correlation of FaMIVE and EMS'98, Stonework

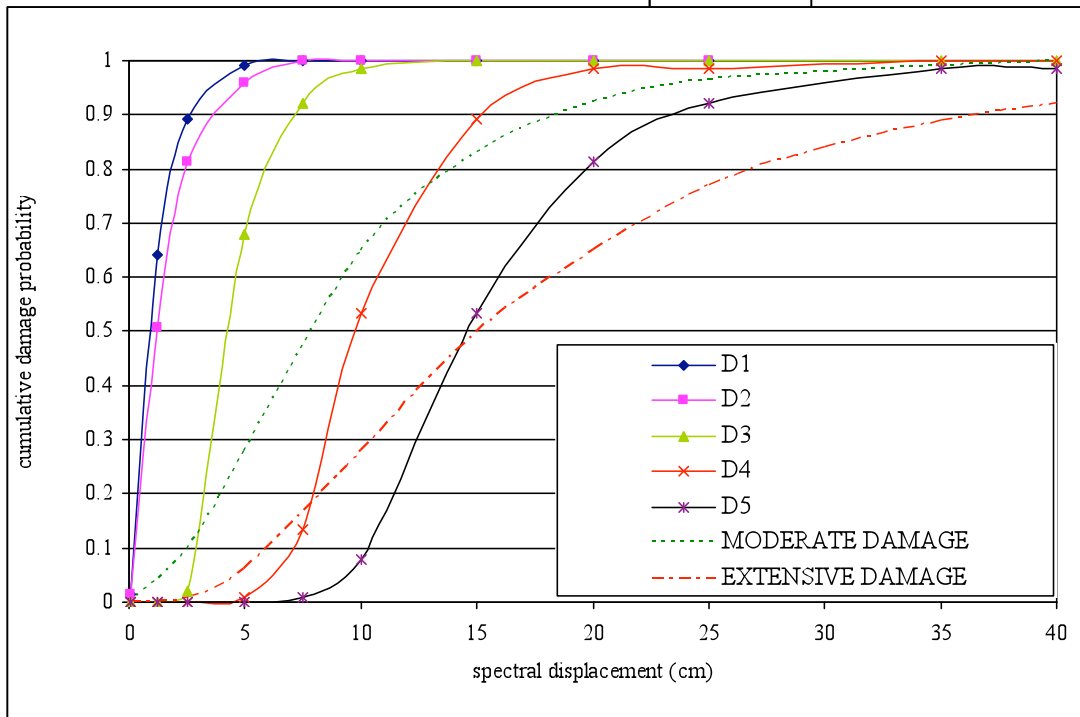
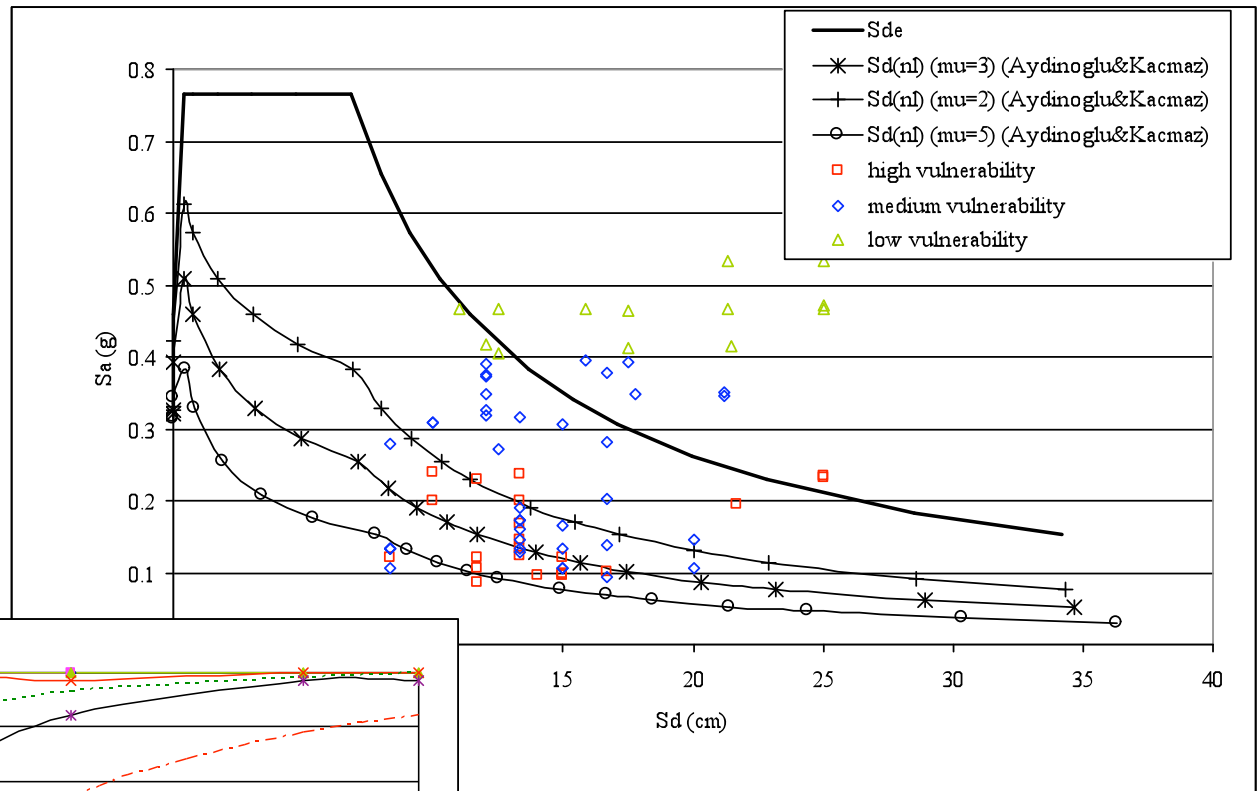
Procedure	EMS98 grade A	EMS98 grade B	EMS98 grade C
VULNUS	High and Very High	Medium	Low and Very Low
FaMIVE	Extreme and High	Medium	Low



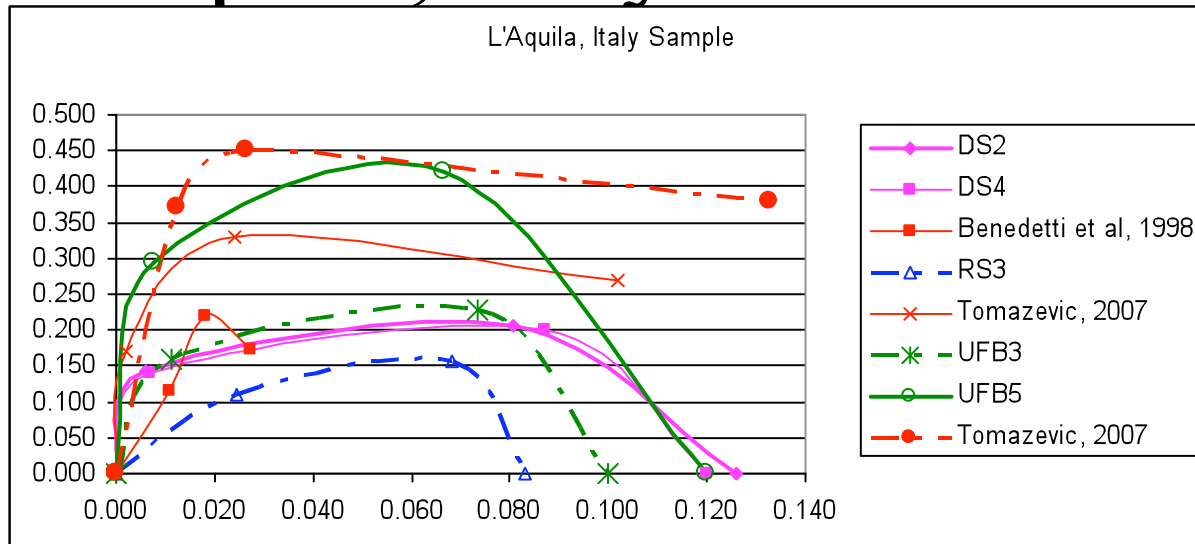
Turkey, Fener-Balat



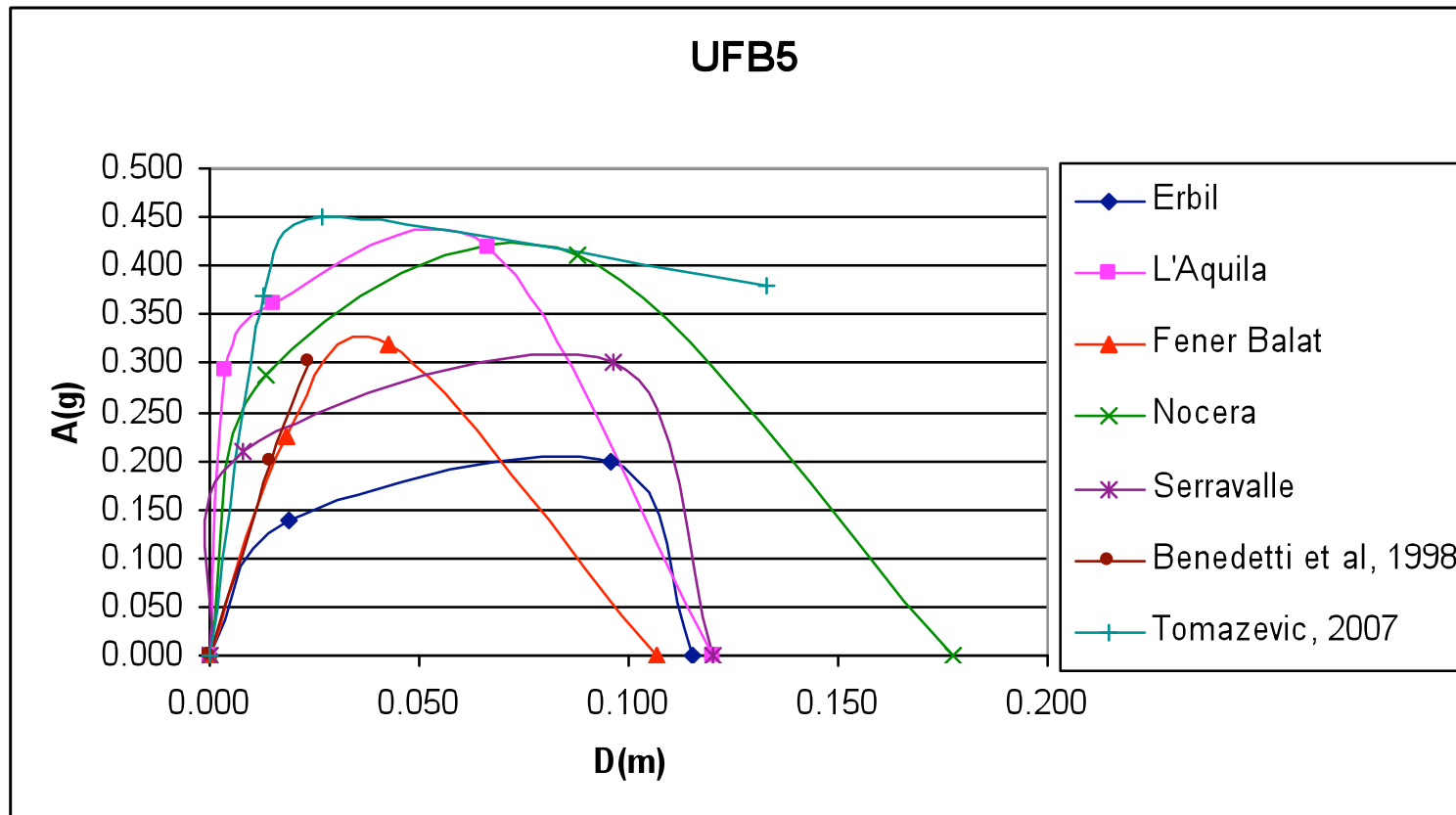
Displacement based damage scenario



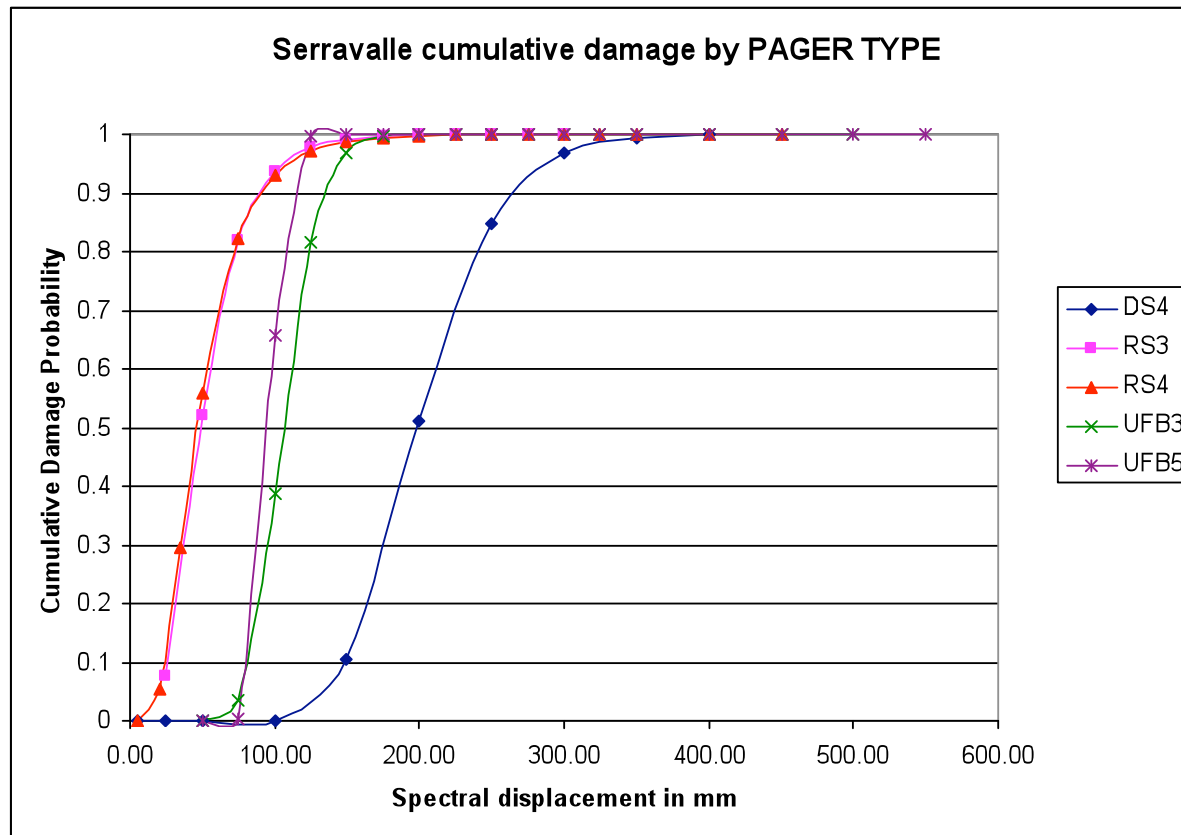
L'Aquila, Italy



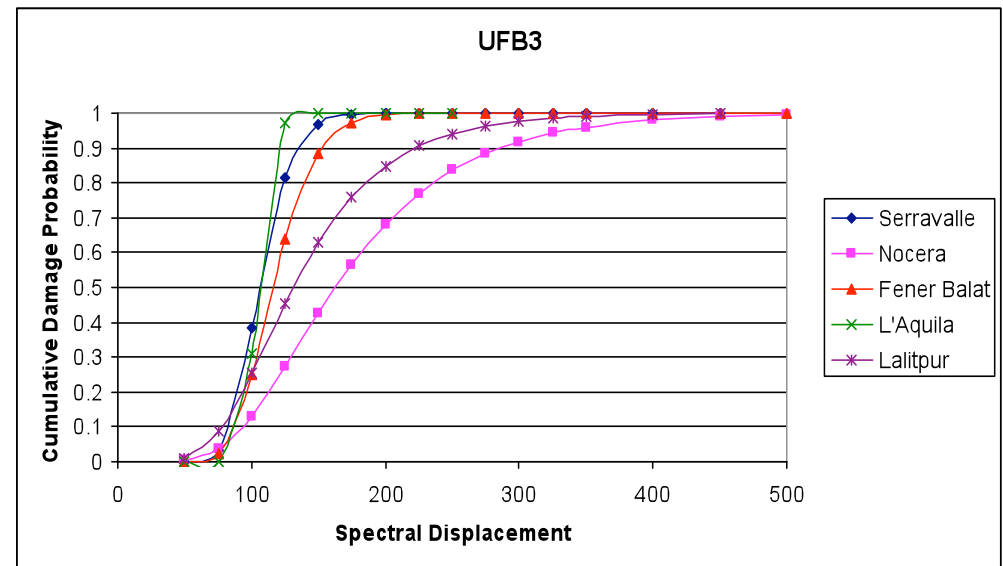
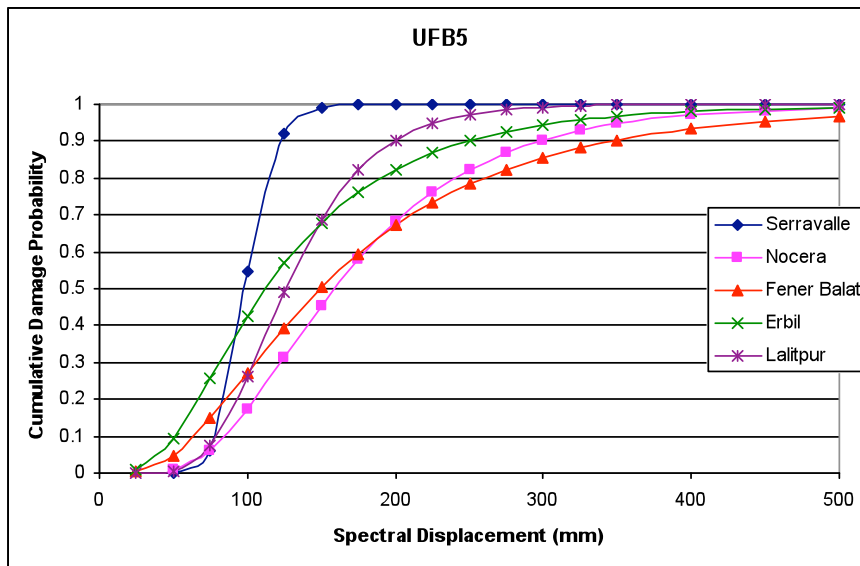
Comparison FaMIVE experimental for UFB5



Cumulative total damage probability

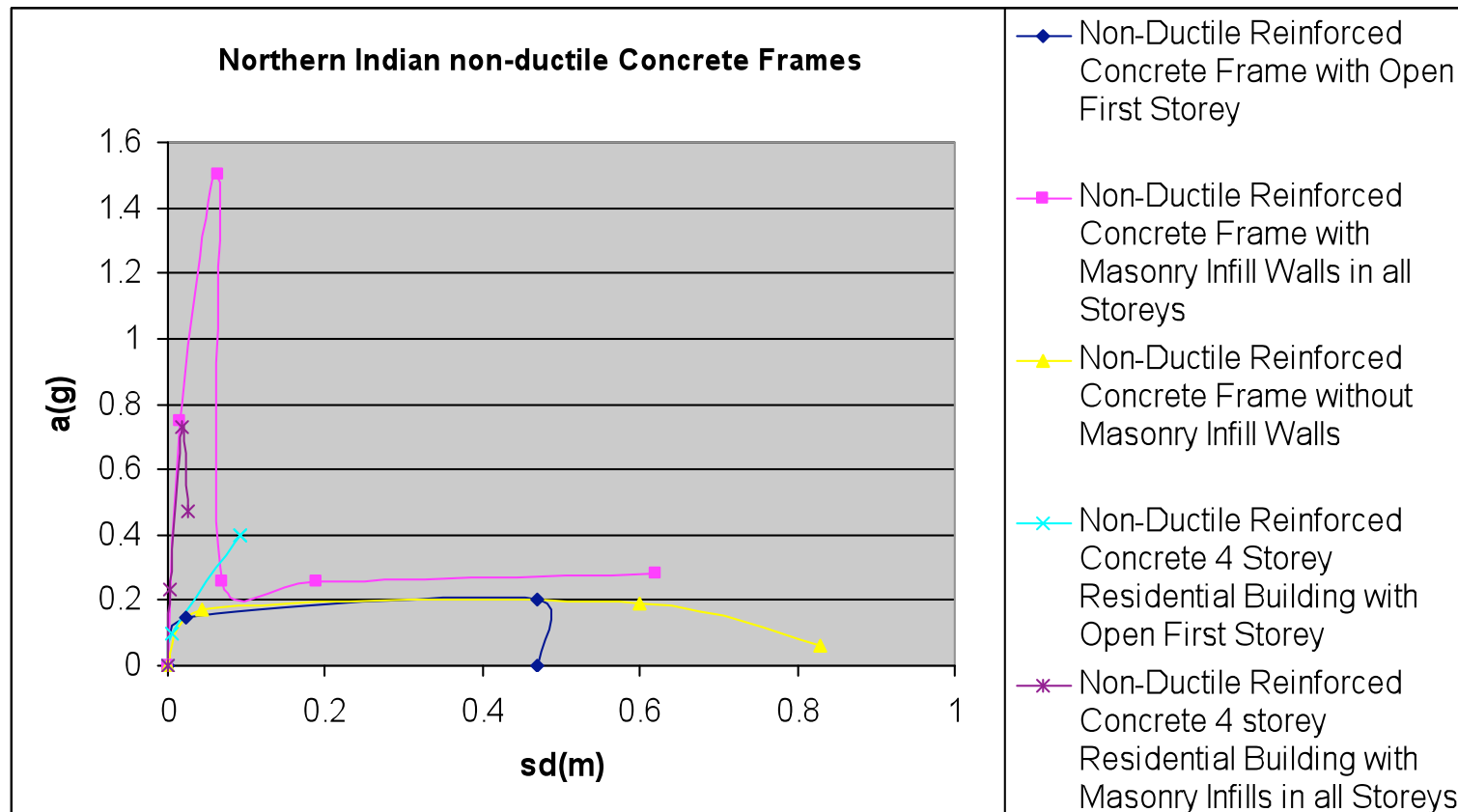


Cumulative distribution over the whole sample for UFB3 and UFB5

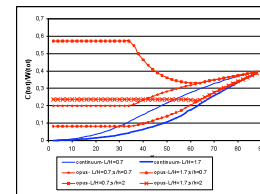
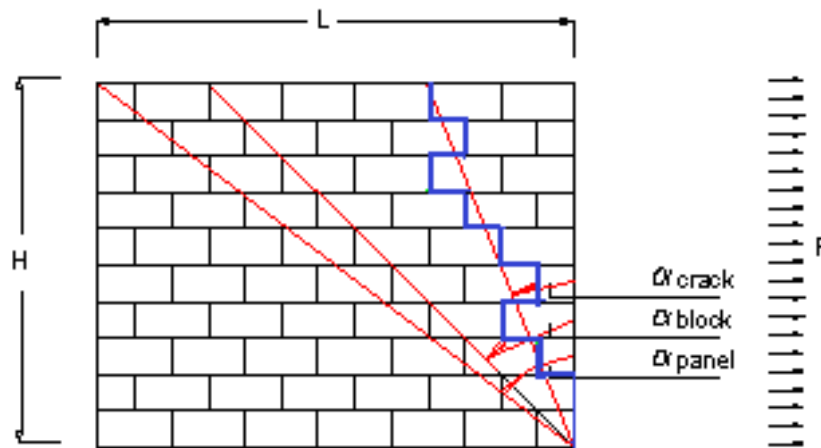
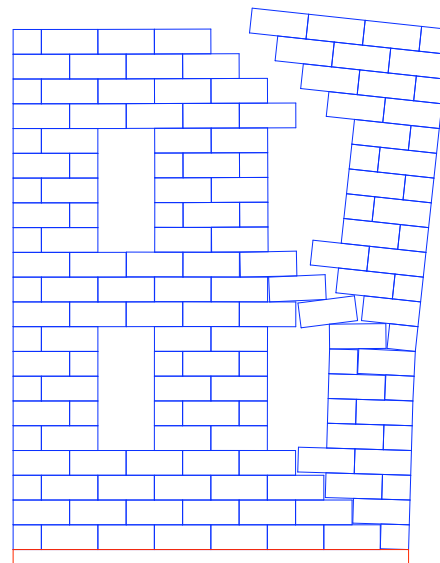
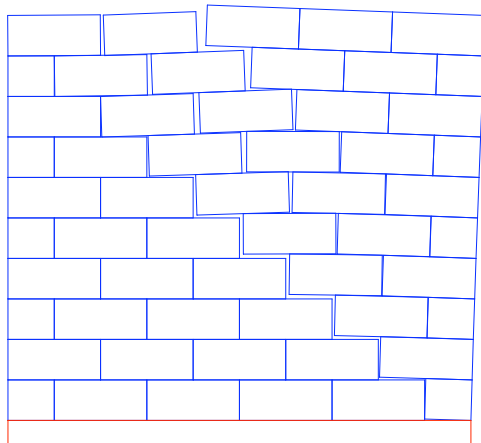


Indian Data Concrete structures

C3M



Friction model



Input: electronic survey form



INSPECTION FORM FOR THE SURVEY OF ORDINARY BUILDINGS

Town Build. Cad. sheet Type of use Date
 Address Particel n. % of use Surveyor

1 URBANISTIC DATA reliability --->

1-1 Block access and escape routes 1-4 Position of building within the block
 1-2 Shape and composition of the block 1-5 Connection of façade to adjacent walls
 1-3 Number of buildings in the block 1-6 Foundation soil

2 GEOMETRIC CHARACTERISTICS OF THE FAÇADE reliability --->

2-1 Facade orientation 2-5 Total height of the facade
 2-2 Number of storeys of the building 2-6 Presence of gable
 2-3 Number of storeys of the facade 2-7 Gable height (if present)
 2-4 Length of the facade 2-8 Additional corner in the facade

3 GEOMETRIC CHARACTERISTICS OF OPENINGS reliability --->

3-1 Number of openings per storey 3-3 Openings layout
storeys
disp. n.s.
left right
 3-4 Lateral pier
 openings
b h
 3-5 Height of upper horizontal spandrel
type Length Material
 3-2 Average opening dimensions 3-6 Lintel

4 PLAN GEOMETRIC CHARACTERISTICS reliability --->

4-1 Thickness at basis of facade wall 4-4 N. int. bearing walls // to the facade
 4-2 Thickness reduction at the top (%) 4-5 Total length perp. to the facade
 4-3 N. int. bearing walls perp. to facade 4-6 internal wall perp. to back façade

5 STRUCTURAL CHARACTERISTICS reliability --->

5-1 N. storeys with vaulted structures 5-7 Level of maintenance of masonry
left right
 5-2 Horizontal structure typology 5-8 Connection at edges
 5-3 Direction of hor. Structure 5-9 Out of verticality
 5-4 Roof structure typology 5-10 pegs/wall plate/timber bands
 5-5 Direction of roof
 5-6 Masonry type
 5-6b mortar type

storey	4	3	2	1	0
pegs		4			
wall plate		A2	A2	A2	
timber bands					

6 FURTHER VULNERABILITY ELEMENTS reliability --->

6-1 Presence of vertical addition 6-3 Specific weight alteration% (+/-)
H t
 6-2 Dimensions of vertical addition 6-4 Chimney flue within the façade wall
L no. of struts
 6-5 Roof overhanging 6-6 Settlement
L t no. of stories
 6-7 Jetting out 6-8 Presence of dalan
L no. of pillars

7 DAMAGE LEVEL AND MECHANISMS IDENTIFICATIONS reliability --->

7-1 Mechanisms identification

Class	Type	D. level
A	<input type="text"/>	<input type="text"/>
B	<input type="text"/>	<input type="text"/>
C	<input type="text"/>	<input type="text"/>
D	<input type="text"/>	<input type="text"/>
E	<input type="text"/>	<input type="text"/>
F	<input type="text"/>	<input type="text"/>
G	<input type="text"/>	<input type="text"/>
H	<input type="text"/>	<input type="text"/>
I	<input type="text"/>	<input type="text"/>
L	<input type="text"/>	<input type="text"/>
Other kind of damage or failure not identified <input type="text"/>		

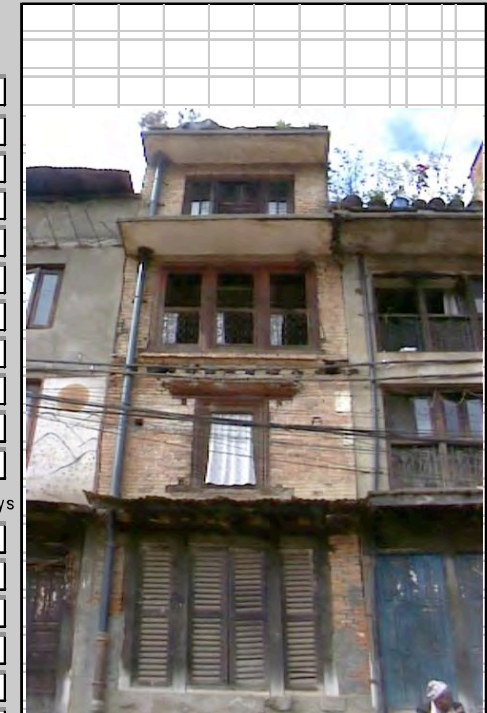
7-2 Crack pattern description no of storeys

Horizontal cracks	<input type="text"/>	<input type="text"/>
Vertical cracks	<input type="text"/>	<input type="text"/>
Corner cracks	<input type="text"/>	<input type="text"/>
Diagonal cracks	<input type="text"/>	<input type="text"/>
Masonry failure	<input type="text"/>	<input type="text"/>

7-3 Damage extention (% of facade)
Year

7-4 Earthquake damage

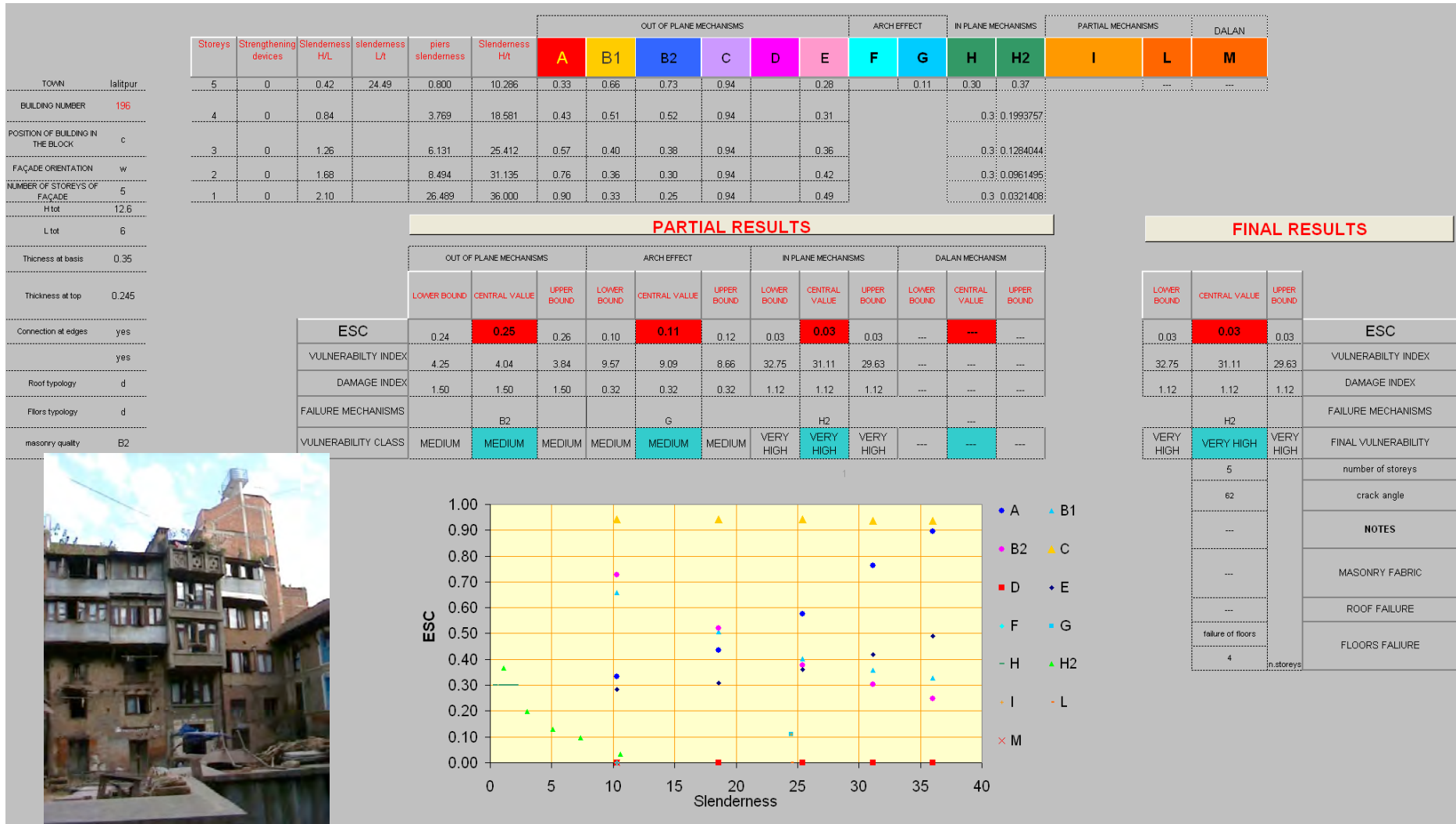
Notes

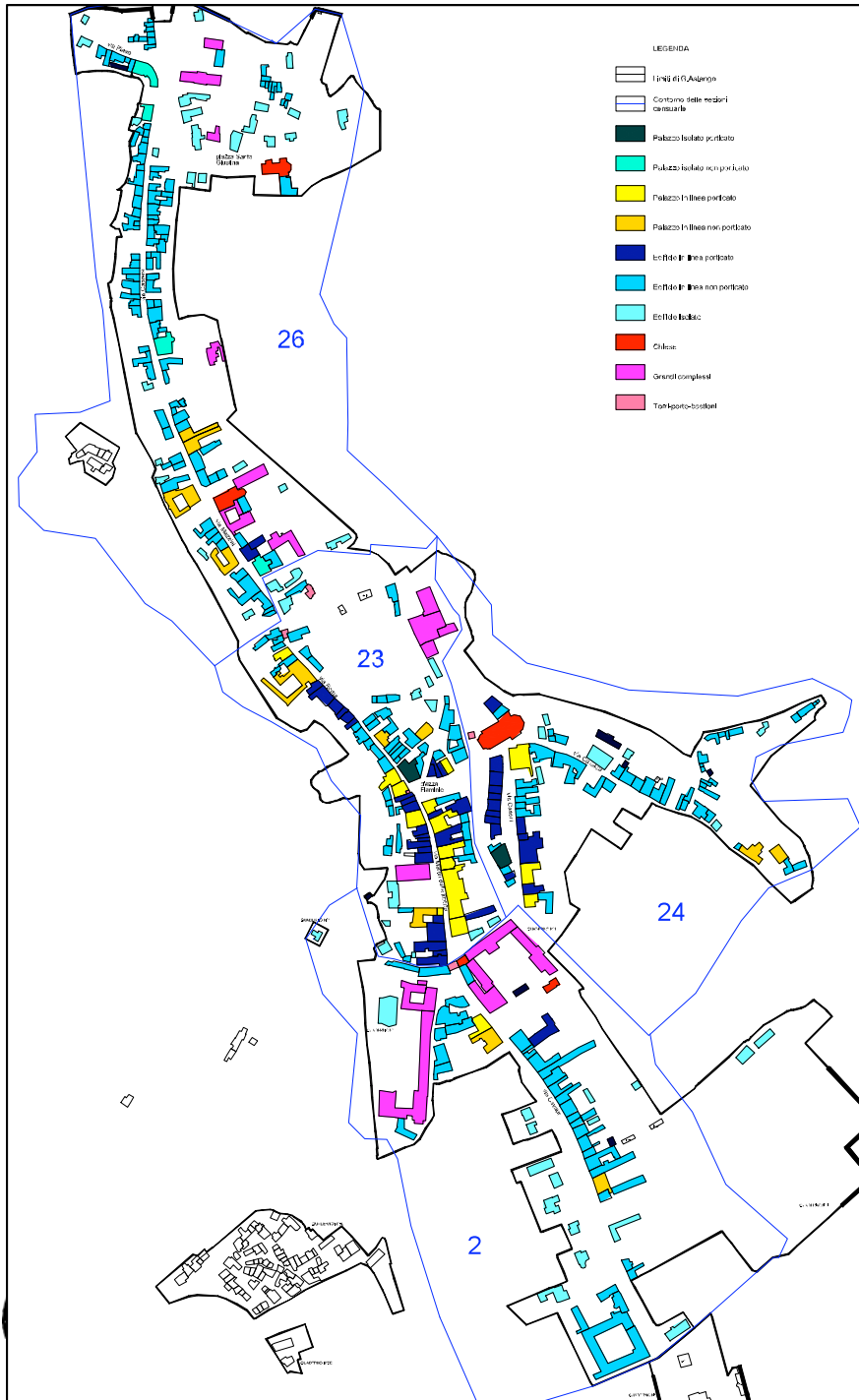


Output for one façade



Earthquake Engineering
Research Institute



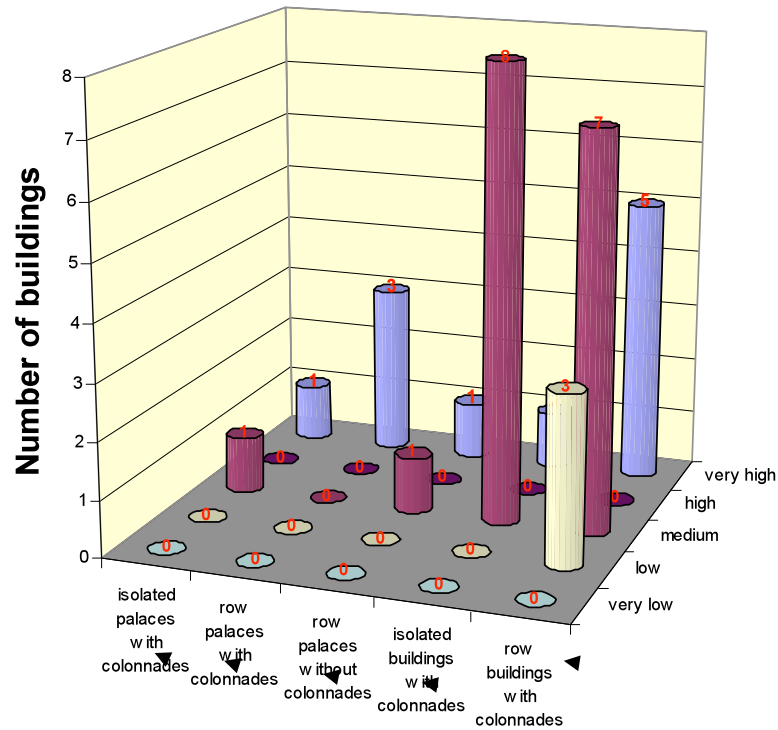


**CLASSIFICATION OF
BUILDING TYPOLOGIES in
Vittorio Veneto**

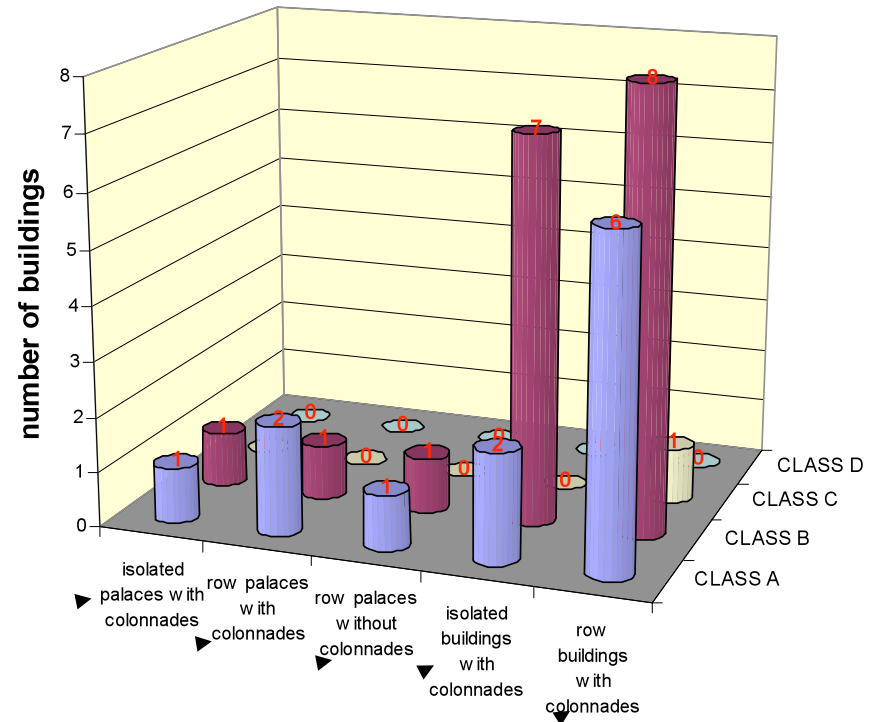
Serravalle

VULNERABILITY (VULNUS) and EMS 98 VULNERABILITY Class for different Typologies

Comparison VULNUS-typologies ($a/g=0.16$)



Comparison EMS98-typologies



Conclusions

- Traditional buildings are generally classified as class B of the EMS98 with subset in class A when structural deficiencies are present, and subset in class C when strengthening is effective.
- It is feasible to use a consistent structural approach to define fragility curves for force based vulnerability assessment by typologies.
- It is also feasible to derive a displacement based vulnerability analysis using ultimate displacement capacity and demand. This highly relies on accurate estimate of ductility.
- Such analyses can be used to identify cluster of buildings with deficiency in need of upgrading
- Vulnerability of the single building depends on several variables but most important are elements directly enhancing or reducing vulnerability and allowing or preventing collapse mechanisms, hence direct observation is essential
- Accurate analysis of the structural details in a given building sample allows to identify indigenous strengthening techniques which are effective and organic
- Comparison with EMS98 and HAZUS curves show that FAMIVE classes are more homogenous and do not necessarily respond to normal distribution models.
- For the brickwork good constructional details correlation is shown among samples in Nepal and Turkey, for instance, providing some scope for generalisation.
- For stone masonry performance is more strictly related to fabric quality hence more difficult to generalise.